

Series lectures of phase-field model

02. Therodynamic anaysis of diffusion

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Diffusion in substitutional alloys

In binary substitutional alloys, the rate at which solvent (A) and solute (B) atoms can move into a vacant site is not equal, therefore, we have to know **intrinsic** diffusion coefficient D_A or D_B . D_A and D_B are defined such that Fick's first law applies to diffusion relative to the lattice

$$J_A = -D_A \frac{\partial c_A}{\partial x} \quad (1)$$

$$J_B = -D_B \frac{\partial c_B}{\partial x} = D_B \frac{\partial c_A}{\partial x} \quad (2)$$

When $D_A > D_B$, we have

$$|J_A| > |J_B|$$

Another main assumption is the volume of the system is constant. To achieve it, the flux have to be balanced. Since the direction of A atom flux and B atom flux are opposite.

$$-J_A = J_B + J_V \quad (3)$$



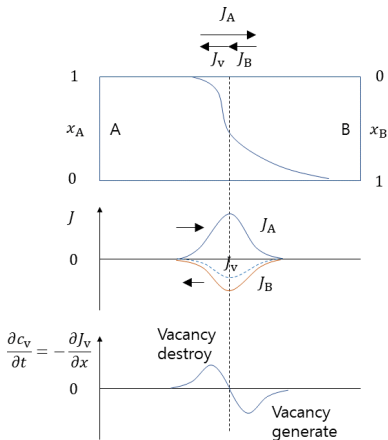


Figure: Interdiffusion and vacancy flow

With Eqs. 1, 2 and 3 we have

$$J_v = (D_A - D_B) \frac{\partial c_A}{\partial x} \quad (4)$$



The velocity at which any given lattice plane moves, v , the plane where the area is A , during a small time interval δt . The plane sweep out a volume

$$Av \cdot \delta t$$

containing

$$Av \cdot \delta t \cdot c_0$$

atoms. This number of atoms is removed by the total number of vacancies crossing the plane in the same time interval,

$$J_v A \cdot \delta t$$

Therefore,

$$J_v = c_0 v \quad c_0 = c_A + c_B$$

Then Eq. 4 becomes

$$v = (D_A - D_B) \frac{\partial X_A}{\partial x} \quad (5)$$

where the mole fraction of A,

$$X_A = \frac{c_A}{c_0}$$



We introduce the concept of total flux of A which is combined effect of (i) diffusive flux relative to the lattice and (ii) flux due to the velocity of lattice

$$J'_A = -D_A \frac{\partial c_A}{\partial x} + v c_A$$

With Eq. 5,

$$\begin{aligned} J'_A &= -D_A \frac{\partial c_A}{\partial x} + (D_A - D_B) \frac{\partial X_A}{\partial x} \cdot c_A \\ &= -D_A \frac{\partial X_A}{\partial x} \cdot \underbrace{c_0}_{c_A + c_B} + (D_A - D_B) \frac{\partial X_A}{\partial x} \cdot c_A \\ &= -(D_A c_B + D_B c_A) \frac{\partial X_A}{\partial x} \\ &= -(D_A X_B + D_B X_A) \cdot c_0 \frac{\partial X_A}{\partial x} \\ &= -\underbrace{(D_A X_B + D_B X_A)}_{\tilde{D}} \cdot \frac{\partial c_A}{\partial x} \end{aligned}$$



The interdiffusion coefficient \tilde{D} is defined by

$$\tilde{D} = D_A X_B + D_B X_A \quad (6)$$

which is known by Darken's equation. Then Fick's first law becomes

$$J'_A = -\tilde{D} \frac{\partial c_A}{\partial x} \quad (7)$$



Atomic mobility

In a multi-component condensed phase, it is more convenient to describe that atoms diffuse as the gradient of chemical potential becomes the driving force, rather than describing that atoms diffuse as the gradient of concentration becomes the driving force.

$$J_B = v_B c_B$$

Drift velocity is now given by

$$v_B = -M_B \frac{\partial \mu_B}{\partial x}$$

Then, the flux is given by

$$\begin{aligned} J_B &= -M_B c_B \frac{\partial \mu_B}{\partial x} = -M_B c_B \frac{d\mu_B}{d \ln X_B} \frac{\partial \ln X_B}{\partial x} \\ &= -M_B c_0 \frac{d\mu_B}{d \ln X_B} \frac{\partial X_B}{\partial x} = -M_B \frac{d\mu_B}{d \ln X_B} \frac{\partial c_B}{\partial x} \end{aligned} \quad (8)$$



Thermodynamic factor of diffusion coefficient

The chemical potential of atom B is

$$\mu_B = \mu_B^\circ + RT[\ln \gamma_B + \ln X_B]$$

then

$$d\mu_B = RT[d \ln \gamma_B + d \ln X_B]$$

proceed to

$$\frac{d\mu_B}{d \ln X_B} = RT \left[1 + \frac{d \ln \gamma_B}{d \ln X_B} \right] \quad (9)$$

Plug Eq.9 to Eq.8, then

$$J_B = -M_B RT \left[1 + \frac{d \ln \gamma_B}{d \ln X_B} \right] \frac{dc_B}{dx}$$

Compare to Fick's first law,

$$D_B = M_B RT \left[1 + \frac{d \ln \gamma_B}{d \ln X_B} \right]$$



Consistently,

$$D_A = M_A RT \left[1 + \frac{d \ln \gamma_A}{d \ln X_A} \right]$$

For dilute solution, we can approximately state

$$D_B^* = M_B RT$$

$$D_A^* = M_A RT$$

We introduce the thermodynamic factor F ,

$$F = 1 + \frac{d \ln \gamma_B}{d \ln X_B}$$

From Gibbs-Duhem relation with trivial modifications,

$$\frac{d \ln \gamma_A}{d \ln X_A} = \frac{d \ln \gamma_B}{d \ln X_B}$$

The thermodynamic factor F is

$$F = 1 + \frac{d \ln \gamma_B}{d \ln X_B} = 1 + \frac{d \ln \gamma_A}{d \ln X_A}$$

also

$$D_B = F D_B^* \quad D_A = F D_A^*$$

From dG is

$$dG = \mu_A dX_A + \mu_B dX_B$$

then

$$\begin{aligned} \frac{dG}{dX_A} &= \mu_A + \mu_B \frac{dX_B}{dX_A} = \mu_A - \mu_B \\ &= \mu_A^\circ + RT \ln \gamma_A + RT \ln X_A - \mu_B^\circ - RT \ln \gamma_B - RT \ln X_B \end{aligned}$$

Take another differentiation,

$$\frac{d^2G}{dX_A^2} = RT \frac{d \ln \gamma_A}{dX_A} + \frac{RT}{X_A} + RT \frac{d \ln \gamma_B}{dX_B} + \frac{RT}{X_B} = \frac{d^2G}{dX_B^2}$$

Proceed to

$$\frac{X_A X_B}{RT} \frac{d^2G}{dX_A^2} = \left[X_B \left(1 + \frac{d \ln \gamma_A}{d \ln X_A} \right) + X_A \left(1 + \frac{d \ln \gamma_B}{d \ln X_B} \right) \right] = (X_A + X_B) F = F$$

Finally, we reach

$$F = \frac{X_A X_B}{RT} \frac{d^2G}{dX_A^2} = \frac{X_A X_B}{RT} \frac{d^2G}{dX_B^2}$$

Eq. 6 can be rewritten by

$$\tilde{D} = F(X_B D_A^* + X_A D_B^*)$$

In similar logic, we have

$$\tilde{M} = c_{ACB} (M_{ACB} + M_{BCA}) \quad (10)$$